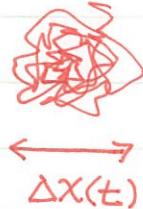


HH0046 Fick's Law For Diffusion

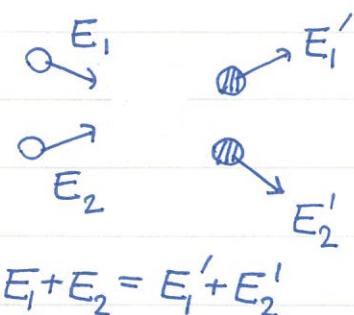
Diffusion in equilibrium — Due to frequent collisions, a molecule's trajectory is rather random,



$$\Delta x(t) = \sqrt{\langle x^2(t) \rangle - \langle x(t) \rangle^2} = \sqrt{\langle x^2(t) \rangle} \propto t^{\frac{1}{2}}$$

The slow spreading of $\Delta x \sim \sqrt{t}$ is called diffusion.

Note that the microscopic collisions not only cause diffusive dynamics but also explain the Boltzmann distribution in equilibrium.



In equilibrium, the transition rate vanishes according to detail balance

$$P(E_1)P(E_2) = P(E'_1)P(E'_2)$$

$\gamma = \gamma'$ by time-reversal symmetry.

It means $P(E)P(E_0-E) = \text{const.}$

OR $\log P(E) + \log P(E_0-E) = \text{const.}$

Differentiate with respect to E ,

$$\frac{d \log P}{dE} \Big|_E - \frac{d \log P}{dE} \Big|_{E_0-E} = 0$$

Since E and E_0-E are arbitrary,

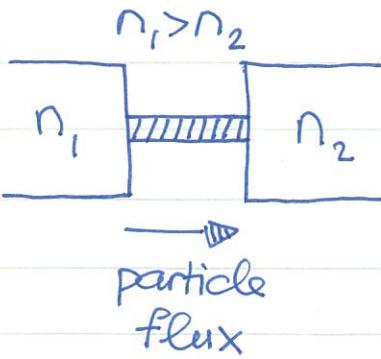
$$\frac{d \log P}{dE} = C$$

equilibrium condition.

Thus, $\log P = CE + D$,

$$P(E) = e^C \cdot e^{DE}$$

Boltzmann distribution.



Now consider diffusion in non-equilibrium yet steady state. From empirical observations,

$$(\text{particle Flux}) \propto (n_1 - n_2)$$

density diff
not too large

Let us be more precise and introduce the flux density of some quantity A:

$$\vec{J}_A = \text{flux density of } A \Rightarrow |\vec{J}_A| =$$

MAX
net quantity of A transported
across unit area in unit time

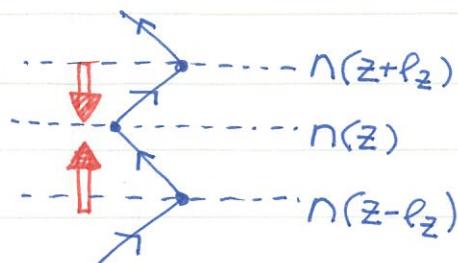
What about the direction? $\hat{\vec{J}_A}$ is the direction of the unit area when the net transported quantity reaches maximum!

For isothermal diffusion, we find that

$$\vec{J}_n = -D \vec{\nabla} n$$

Fick's law: D is the diffusion constant.

Let's try to find a microscopic explanation of Fick's law.



Assume molecules reach local thermal equilibrium after collisions \rightarrow local density $n = n(z)$ may be different.

$$J_n^z = \frac{1}{2} n(z-p_z) \cdot \bar{C}_z$$

upward flux

$$- \frac{1}{2} n(z+p_z) \cdot \bar{C}_z$$

downward flux

If the mean free path ℓ is short,

$$J_n^z \approx \frac{1}{2} \bar{C}_z \frac{dn}{dz} \cdot 2\ell_z = - \bar{C}_z \ell_z \frac{dn}{dz}$$

average over the hemisphere,

$$\langle \bar{C}_z \ell_z \rangle_{\text{hemi}} = \bar{C} \ell \cdot \frac{1}{2\pi} \int_0^{2\pi} d\phi \int_0^{\frac{\pi}{2}} \sin\theta d\theta \cdot \cos^2\theta = \frac{1}{3} \bar{C} \ell$$

where $\bar{C}_z = \bar{C} \cos\theta$, $\ell_z = \ell \cos\theta$. Finally, we obtain the important relation between \vec{J}_n and n

$$\vec{J}_n^z = - \frac{1}{3} \bar{C} \ell \frac{dn}{dz} \quad \text{i.e.} \quad \vec{J}_n = - D \vec{\nabla} n \quad \text{with } D = \frac{1}{3} \bar{C} \ell$$

① **Thermal conductivity:** We can apply the same idea to heat conduction due to diffusive dynamics. Let us generalize the above derivation for some quantity A .

$$\text{Equilibrium} \rightarrow \vec{J}_A = P_A \langle \vec{v} \rangle = 0$$

$$\text{Steady State} \rightarrow \vec{J}_A = - D \vec{\nabla} P_A \neq 0$$

No drift flow
is considered
in these cases

Suppose the energy density is P_u and its flux density is \vec{J}_u

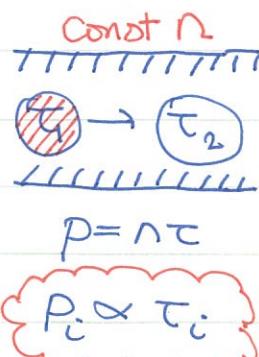
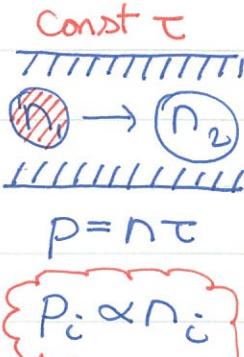
$\vec{J}_u = -D \vec{\nabla} P_u$, note that $\partial_i P_u = \left(\frac{dP_u}{dT}\right) \partial_i T$ by chain rule,

$$\rightarrow \boxed{\vec{J}_u = -K \vec{\nabla} T} \text{ with } K = D \cdot \frac{dP_u}{dT} = D \cdot C_v \quad \text{heat capacity per unit volume.}$$

Thus, the constant K is related to microscopic collisions as well,

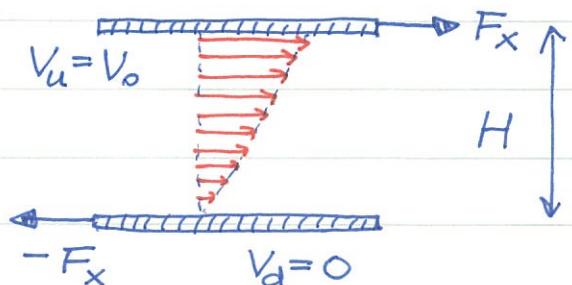
$$K = \frac{1}{3} C_V \bar{C} \ell$$

Particle Flux driven by density gradient is similar to energy Flux driven by temperature gradient.



② **Viscosity**: We now want to view viscosity as consequence of momentum transverse flow.

$$V_x(z) = V_0 \cdot \frac{z}{H} \propto z \quad \frac{dU_x}{dz} \neq 0$$

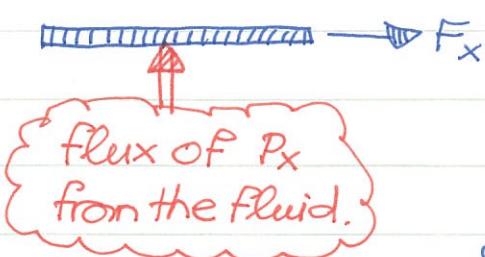


The shear stress is $f_x = F_x/A$

From empirical observations,

$$f_x = -\eta \frac{dU_x}{dz}$$

where η is the viscosity coefficient.
Can this be explained by microscopic collisions as well? Yes!



Since the slab is moving at const velocity,

$$F_x = \text{Flux of } P_x \text{ from fluid}$$

OR

$$f_x = \text{flux density of } P_x \text{ from fluid}$$

Q: What happens to the other slab?

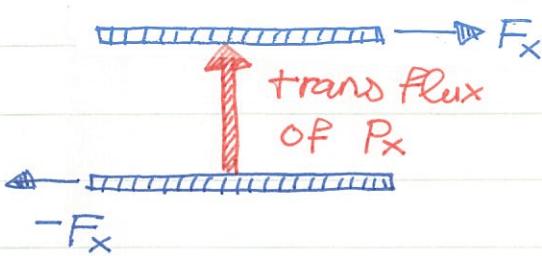
The density of momentum P_x is $\underline{P_x} = n \cdot M v_x$. Thus, the corresponding flux density is $J_{P_x}^z = -D \frac{dP_x}{dz} = -D n M \frac{dv_x}{dz}$

$nM = \rho$ is the mass density, the flux density equals the stress $f_x = J_{P_x}^z$. $f_x = -\eta \frac{dv_x}{dz}$ with $\boxed{\eta = D\rho = \frac{1}{3}\rho \bar{c} e}$

It may seem that the viscosity coefficient η depends on the density. Well, it is not !!

$$\eta = \frac{1}{3} \rho \bar{c} e = \frac{1}{3} \cdot \cancel{n} M \bar{c} \cdot \frac{1}{\cancel{n} \pi d^2} = \frac{M \bar{c}}{3 \pi d^2} \quad \text{indep of density } n !!$$

Now we have a refreshing view on viscosity: The steady state without time dependence is reached



$$\left\{ \begin{array}{l} k = \frac{1}{3} \alpha_v \bar{c} e \\ \eta = \frac{1}{3} \rho \bar{c} e \end{array} \right.$$

→

$$\boxed{F_x = J_{P_x}^z \cdot A} \quad \text{on both slabs.}$$

In addition, there is a relation between k and η .

$$\boxed{\frac{kp}{\eta c_v} = 1}$$

$$\begin{array}{ll} N_2: 1.91 & H_2: 1.91 \\ O_2: 1.90 & He: 2.40 \end{array}$$

The value of $kp/\eta c_v$ is not unity for realistic gases, but close (given our derivation is so rough).



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